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(54) Title: BLOCK COPOLYMERS FROM IONIC CATALYSTS

## (57) Abstract

A process for the production of block copolymers of ethylene and an  $\alpha$ -olefin such as propylene by using an ionic catalyst system including a metallocene component and a component having a cation capable of donating a proton and a compatible non-coordinating anion. Novel block copolymers are produced.

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## APPLICATION FOR PATENT

Title: BLOCK COPOLYMERS FROM IONIC CATALYSTS

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SPECIFICATIONCross-Reference to Related Applications

10        This application is a Continuation-In-Part of  
Copinging USSN 477,791 filed February 9, 1990 which is a  
Continuation-In-Part of copending U.S. Patent Application  
Nos. 133,052 filed December 21, 1987 and 133,480 filed  
December 22, 1987. Copending U.S. Patent Application No.  
15    133,052 is in turn a Continuation-In-Part of U.S. Patent  
Application No. 011,471 filed January 30, 1987.  
Copinging U.S. Patent Application No. 133,480 is in turn  
a Continuation-In-Part of U.S. Patent Application No.  
008,800 filed January 30, 1987 all of which are  
20    incorporated by reference. This application is also  
related to copending USSN 07/917,008.

FIELD OF THE INVENTION

25        This invention relates to a method for preparing  
block and tapered copolymers by polymerizing ethylene and  
other olefins in the presence of an activated  
cyclopentadienyl transition metal catalyst system. More  
particularly, this invention relates to a process for the  
30    production of multiblock and tapered copolymers of  
ethylenically unsaturated monomers. The invention also  
related to the multiblock and tapered copolymers  
produced.

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BACKGROUND OF THE INVENTION

Block copolymers are well known and have been used commercially as components in adhesives, as melt processable rubbers, impact resistant thermoplastics, and as compatibilizers, or "surfactants", for emulsifying polymer-polymer blends.

A block copolymer is created when two or more polymeric segments, or blocks, of different chemical composition are covalently bonded in an end-to-end fashion. Block copolymers have certain advantages over blends. Firstly, the segments are covalently bonded to each other, thereby eliminating the interface problem. Secondly, block copolymers can be used to strengthen blends of immiscible polymers by serving as "emulsifiers," which encourage physical connections between the phase, and thus improve the interfacial adhesion and load transferring capability of the components.

While a wide variety of block copolymer architectures are possible, most block copolymers of interest involve the covalent bonding of hard plastic segments which are crystalline or glassy, to elastomeric blocks forming thermoplastic elastomers. Other block copolymers, such as rubber-rubber, glass-glass, and glass-crystalline block copolymers are also possible and may have commercial importance. Two common types of block copolymer structures are the diblock and triblock forms. However, multiblock copolymers, in which more than three segments are bonded together, are also desirable.

Block copolymers are similar to, yet distinct from, tapered polymers. In a tapered copolymer the composition of comonomer is gradually varied from one end of the polymer to the other. Tapered copolymers are

commercially used as viscosity modifiers, oil additives, thermoplastic elastomers, and impact-resistant plastics.

Block copolymers have been made by anionic  
5 polymerization routes. Butadiene-isoprene block  
copolymers have been synthesized using the sequential  
addition technique. In sequential addition, a certain  
amount of one of the monomers is contacted with the  
catalyst. Once the monomer has reacted to extinction,  
10 forming the first block, a certain amount of the second  
monomer species is introduced and allowed to react to  
form the second block. The process may be repeated as  
desired using the same or other anionically polymerizable  
monomers.

15 Likewise, olefin based block copolymers have not  
been successfully synthesized through coordination  
catalysis. Several difficulties arise in the use of  
known coordination catalysts for the block  
20 copolymerization of olefins. Among those are the fact  
that conventional catalysts are typically multi-sited,  
and a significant fraction of the active sites are  
unstable. This leads to random chain initiation and  
termination which, in turn, lowers the theoretical block  
25 copolymer yield. What is desired, and what practice of  
this invention provides, is a catalyst system with well-  
characterized structure and reactivity which has a single  
active site. The system should have well-defined and  
stable polymerization kinetics and be free of aluminum  
30 alkyls or other chain transfer agents.

#### SUMMARY OF THE INVENTION

The invention comprises a process for the production  
35 of novel block copolymers of ethylene with an  $\alpha$ -olefin  
and the polymers obtained therefrom. The process  
includes sequentially contacting ethylene with an  $\alpha$ -

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olefin monomer in a suitable solvent at 0°C in the presence of an activated cyclopentadienyl catalyst system to produce a block or tapered block copolymer. The activated catalyst will polymerize  $\alpha$ -olefins to form tapered polymers and multiblock polymers such as di- and tri-block homopolymers and copolymers of ethylene and propylene with one or more other alpha-olefins.

#### BRIEF DESCRIPTION OF THE DRAWING

Figure 1 is a graph of the percent insolubles vs. polymerization time in minutes.

Figure 2 is graph of the tensile strength of EP/PP block copolymers at 100 and 120 degrees C.

Figure 3 is a graph of the effect of EP block polymerization time on blocking efficiency.

#### DESCRIPTION OF PREFERRED EMBODIMENTS

The invention provides (1) novel di, tri-, and multi-block copolymers and tapered copolymers of ethylene, 1-olefins, diolefins, cyclic olefins, acetylenes and other unsaturated monomers; and (2) the processes for polymerizing said block copolymers.

#### Activated Catalyst System - General System

The process of this invention is practiced with that class of catalyst referred to, disclosed, and described in U.S. Patents 5,055,438; 5,057,475; 5,096,867; 5,017,714; 5,153,157; copending USSN's 542,236 filed June 22, 1990; 468,382 filed May 21, 1991; 885,170 filed May 18, 1992; 737,611 filed July 19, 1991; 926,006 filed August 5, 1992; 07/133,052 and 07/133,480 and EPA's 277,003, 277,004, published Jun 3, 1988; EPA 129,368

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published December 22, 1984, EPA 520,732 published  
December 30, 1992 all of which are incorporated by  
reference herein. The activated catalyst is prepared by  
combining at least two components. The first of these is  
5 a mono or bis(cyclopentadienyl) derivative of a Group IV-  
B metal compound containing at least one ligand which  
will combine with the second activator component or at  
least a portion thereof such as a cation portion thereof.  
The second component may be an alumoxane or a  
10 noncoordinating anion.

#### Choice of Group IV Metal Component

In general, most Group IVB metal components may be  
15 combined with most activator components to produce an  
active olefin polymerization catalyst.

To obtain block copolymer with a hard segment and a  
soft segment, it is important to choose a catalyst  
20 capable of producing both. For example, a chiral  
activated catalyst will produce stereoregular polyolefins  
while an achiral activated catalyst typically produces  
non-stereoregular, even amorphous polyolefins. As an  
example, a chiral cyclopentadienyl hafnium based catalyst  
25 could be used to produce hard blocks of isotactic  
polypropylene and at different reaction conditions the  
same catalyst could then produce soft "elastomer" blocks  
of EP.

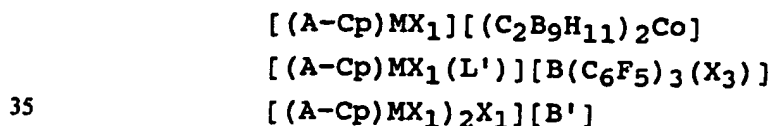
30 Anionic coordination complexes containing  
perfluorophenyl-, trifluoromethylphenyl-, or bis-  
trifluoromethylphenyl rings are preferred. When the non-  
coordinating anion contains a plurality of boron atoms,  
more effective catalysts are obtained with activator  
35 compounds containing larger anions.



Preferred Catalysts for the Production of Block and  
Tapered Copolymers

5 Preferred catalyst systems for the production of  
block copolymers are single-sited living catalysts.  
Living catalysts are those systems in which chain  
transfer is substantially nonexistent and the rate of  
initiation is fast compared to propagation. Catalysts  
10 which have finite chain transfer rates may also be useful  
for the production of block and tapered copolymers if the  
rate of propagation is fast relative to termination. It  
is also important that the average chain lifetimes are  
reasonably long (minutes to hours) in order to permit  
15 adequate time for modifications of the reactor conditions  
(e.g. changing monomer feed streams). While most  
reasonably stable ionic catalysts described above will  
under suitable conditions produce block and/or tapered  
copolymers of nonpolar olefins, it is preferred that the  
20 catalyst be: 1) thermally stable (recoverable as a single  
organometallic complex), 2) versatile in terms of random  
copolymer synthesis (i.e. capable of preparing HDPE, i-  
PP, s-PP, EP-rubber, LLDPE etc.), 3) capable of producing  
high molecular weight polymers at reasonable temperatures  
25 and pressures, 4) high activity (fast propagation  
catalysts) and 5) slow in chain termination reactions so  
that few chains of polymer product are produced per hour  
per site.

30 Preferred activated biscyclopentadienyl catalysts  
are represented by the formulae:



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wherein: M is titanium, zirconium or hafnium; (A-Cp) is either (Cp)(Cp\*) or Cp-A'-Cp\*; and Cp and Cp\* are the same or different substituted or unsubstituted cyclopentadienyl radicals; A' is a covalent bridging group containing a Group IV-A element; L' is a neutral Lewis base; X<sub>1</sub> is a hydride radical, hydrocarbyl radical having from 1 to 20 carbon atoms, substituted-hydrocarbyl radical, wherein 1 or more of the hydrogen atoms are replaced with a halogen atom, having from 1 to 20 carbon atoms, or organo-metalloid radical comprising a Group IV-A element wherein each of the hydrocarbyl substituents contained in the organo portion of said organo-metalloid, independently, contain from 1 to 20 carbon atoms; X<sub>3</sub> is a hydride, halide, hydrocarbyl radical, a C<sub>1</sub> - C<sub>20</sub> hydrocarbyl radical wherein one or more of the hydrogen atoms is replaced by a halogen atoms, organometalloid radical wherein each hydrocarbyl substitution in the organo portion contains from 1 to 20 carbon atoms and the metal is a Group IVA metal and B' is a noncoordinating anion. In another preferred embodiment B' can be replaced with an alumoxane, preferably methylalumoxane. These catalysts are preferred catalysts for the production of block and tapered copolymers of ethylene, 1-olefins, dienes, cyclic olefins and other unsaturated monomers. Ionic catalysts of this form where M= Hf are the most preferred. Polymerizations using hafnium systems of this form under standard random copolymer conditions as described in our copending U.S. Patent Application No. 133,480 produce high molecular weight HDPE, LLDPE, a-PP, i-PP, s-PP, and EP-rubber at rates comparable to similar Zr-based catalysts. In another embodiment on of the Cp rings could be replaced by a heteroatom ligand as described in US 5,055,438, incorporated by reference above. Tapered and block copolymers containing the above segments can be produced using the appropriate hafnium ionic catalysts using the

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techniques and process conditions set forth in the following sections.

Processes for the Production of Block and Tapered  
Copolymers

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15  
Many procedures for modifying the reactor conditions and monomer feeds for the production of block copolymers have been developed and applied using conventional Ziegler-Natta catalysts. The processes include batch reactors and sequential additions techniques, series batch reactors, loop and tubular reactors, and fluidized bed reactors. A review of the processes and patents is given in chapter 4 of "Block Copolymers" [D. C. Allport and W. H. James; John Wiley and Sons, New York 1973]. In principle, the catalysts of this invention can be used in any of the processes described above for the production of well-defined block copolymers.

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The most demanding process, that is the process which requires the longest chain lifetimes, is sequential addition. In the first step of the sequential addition process, the catalyst is placed in a well stirred batch reactor in a suitable solvent and first segment of the block copolymer is grown by adding a specific number of molar equivalents of monomer(s). The catalyst consumes all of the monomer(s) prior to addition of the second monomer(s) (a different set of monomers than in the first step). This procedure can be repeated to prepare multiblock copolymers. As an added step the polymerization vessel can be vacuumed free of substantially all leftover monomer or vented of monomer and/or purged with nitrogen or other suitable inert dry gases in between some or all of the monomer addition steps.

### Sequential Addition Conditions: Solvent

Preferably, the solvent should normally disperse or  
5 dissolve the catalyst to form a well-mixed system. The  
most preferred catalysts for block copolymer synthesis,  
(ACpHfMe(L'))[B(C<sub>6</sub>F<sub>5</sub>)<sub>4</sub>], are prepared in toluene and form  
non-miscible, toluene-dispersible phases. The  
concentration of toluene in the catalyst phase depends on  
10 temperature and the structure of the catalyst. While  
aliphatic hydrocarbons, fluorinated hydrocarbons, and  
chlorinated aromatic hydrocarbons may be used in this  
invention, the preferred solvents for the preparation of  
block copolymers from the most preferred catalysts are  
15 aromatic hydrocarbons such as toluene, xylene, ethyl  
benzene and the like.

### Temperature

20 The reactor temperature strongly affects the yield  
of block copolymer and must be adjusted depending on the  
type and concentration of monomers and catalyst used.  
The general procedure for determining this condition is  
to 1) find the maximum temperature where high molecular  
25 weight polymer segments can be prepared and 2) confirm  
the molecular weight is controlled by the catalyst-to-  
monomer ratio at this temperature. The general trend is  
that higher temperatures cause chain transfer to be more  
rapid relative to propagation and therefore give lower  
30 block copolymer yields. The process may be carried out  
at temperatures of -80°C to 80°C, however, it is  
preferred that the temperature be in the range of -10°C  
to 20°C.

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### Concentration of Catalyst

The concentration should be high enough to produce significant rates of polymerization under the generally low pressure conditions of sequential addition. The concentration should not be so high as to produce uncontrollable exotherms upon exposure to the monomer. The exotherm can be controlled, however, by adjusting the rate of monomer addition during the formation of a block segment. This level of control allows for a large range of acceptable catalysts concentrations. The process may be carried out at catalyst concentrations ranging from  $6 \times 10^{-6}$  to  $6 \times 10^{-2}$  moles of catalyst/liter of solution, however it is preferred that catalyst levels be in the range of  $1 \times 10^{-4}$  to  $3 \times 10^{-3}$  moles of catalyst/liter of solution.

### Monomer Concentration

The amount of monomer added depends on the molecular weight of the targeted polymer and the moles of active catalyst in the reactor. Molar ratios of monomer to catalyst may be in the range of 10:1 to 10,000:1. The monomers may be added quickly or may be metered in to the reactor to control exotherms.

### Order of Monomer Addition

Precipitation of polymer (with catalyst attached) causes undesirable broadening of the molecular weight distribution due to mass transport limitations and poor mixing. It is therefore preferred to prepare the soluble block (generally the elastomeric segment) in the first stage of the reaction. Thus, as indicated in the examples, when ethylene is added in the first step in the synthesis of a HDPE-b-atactic-PP diblock copolymer the

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initially formed polyethylene precipitates with the catalyst and the final molecular weight distribution of crude block copolymer product is rather broad ( $M_w/M_n = 3.0$ ). Addition of propylene in the first step produces a system which remains homogenous throughout the block copolymer synthesis, yielding a crude product having a much narrower  $M_w/M_n = (1.7-1.8)$ .

#### Method of Monomer Addition

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Monomer may be added and removed in such a way that the resulting block copolymer has excellent properties, such as blocking efficiency. This is accomplished by applying a 5 to 10 psi ( $\sim 34$  kPa to  $\sim 69$  kPa) vacuum and purging the reactor with a dry inert gas, such as nitrogen, between monomer addition steps. In a preferred embodiment a minimum vacuum needed is 5 psi. The dry inert gas purge may be at 5 psi or above, preferably at or above 15 psi even more preferably between 5 and 25 psi in a two liter reactor. As is well known to those of ordinary skill in the art the pressures will vary with the size and other conditions of the reactor. Thus these numbers are a guide and not meant to be absolute.

25

#### Preparation of Tapered and Random Copolymers

Addition of stoichiometric amounts of a mixture of two olefins to the reactor under block copolymer conditions will naturally produce tapered copolymer because the monomers will generally have different reactivities with the catalyst. Thus, the head of the polymer will be rich in the more reactive comonomer while the polymer tail will contain larger amounts of the slower reacting comonomer. The extent of tapering will depend on magnitude of the difference of monomer reactivity. The extent of tapering can be controlled by

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metering the two monomers into the reactor at different rates.

Random copolymers such as non-crystalline ethylene-propylene rubber can be made under block copolymer conditions by adding the fast monomer (ethylene) to the catalyst/propylene mixture at a rate where the desired amount of ethylene has been added when all the propylene has been consumed. This procedure is exemplified for a ethylene-propylene elastomer containing 50 mole % propylene.

In a preferred embodiment, tapered block copolymers having properties typical of thermoplastic elastomers (TPE's) can be produced. These particular tapered block copolymers typically strong and elastic, having a low modulus at low strain, high tensile strengths, up to 2500 psi or more, and a tension set of 14 to 25. These tapered copolymers are also characterized by an ethylene content of 15 to 25 mole %, preferably 18 to 23 mole %. These tapered block copolymers can be produced by using a chiral hafnium catalyst, such as those used in the examples below, at a reaction temperature of -10 degrees C to 20 degrees C, preferably -5 degrees C to 10 degrees C. However, higher temperatures could be used, depending on the heat dissipation system utilized. These tapered block copolymers apparently have long stereoregular segments of crystalline polypropylene that are probably formed when the concentration of ethylene in the feed drops to a low level. The DSC melting curves of these polymers typically show a broad melting peak with a sharp crystallization peak at low temperatures.

#### Block Copolymer Products

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The novel polymer products of this invention are olefinic block and tapered copolymers having narrow

molecular weight distributions and well defined di-, tri-, multiblock or tapered structures. The polymer segments which can be incorporated into these architectures include 1) elastomers such as atactic polypropylene, atactic poly-1-olefins, and ethylene/1-olefin copolymers wherein the ethylene comonomer is a C<sub>3</sub>-C<sub>18</sub> 1-olefin such as ethylene-propylene, ethylene butene, and ethylene-octene copolymers ethylene-propylene-diene terpolymers and other crosslinkable elastomeric olefins; 2) thermoplastics such as high density polyethylene, linear low density polyethylene having melting points from 80-135°C (e.g. ethylene-propylene and other ethylene-1-olefin copolymers wherein each 1-olefin has from 4 to 20 carbon atoms), ethylene/diene copolymers such as ethylene/ethyldiene-norbornene copolymers, isotactic polypropylene having melting points from 100°C-165°C, syndiotactic polypropylenes having melting points from 100°C-165°C, semi-isotactic polypropylenes and other crystalline 1-olefin homo and copolymers; and 3) glasses such as homo-polycyclopentene, homopolynorbornene and the like. The average molecular weight of the polymer segments included in the novel block copolymers of this invention can be in the range of from 100-1,000,000 daltons, preferably from 30,000 to 200,000 daltons. The molecular weight distributions (Mw/Mn) of the crude and/or fractionated block copolymer are preferably 5 or less, even more preferably 3 or less, even more preferably 2.5 or less, and even more preferably 2 or less. As indicated above and in the examples following the percentage of block copolymer in the crude product can vary from 1% to 100%, preferably from 50% to 90% depending on the application and the conditions of the experiment. Furthermore, preferred block copolymers of this invention have blocking efficiencies of 30% or greater, preferably 50% or greater, more preferably 70% or greater, even more preferably 90% or greater, and most preferably 95% or greater. In a preferred embodiment



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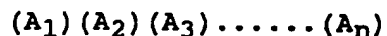
shorter reaction times and lower reactor temperatures are used to produce block copolymers having enhanced blocking efficiency.

5           The block copolymers of this invention can also be formulated into a wide variety of adhesives by blending the block copolymers with one or more solid or liquid tackifiers and optionally other known components such as oils, plasticizers, fillers, antioxidants, coloring  
10   agents, and the like. Useful tackifiers include natural rosins, hydrogenated or non-hydrogenated linear, branched or cyclic aliphatics or aromatics and mixtures thereof. The tackifiers may be present at from 5 weight percent to 95 weight percent based upon the weight of the  
15   composition. Fillers and other additives may be present at up to 150 weight percent based upon the weight of the copolymer and the tackifiers.

          The block copolymers may also be molded or shaped  
20   into articles such as bumpers, shoe soles, dash boards, automotive parts, containers, sheeting and the like by methods known in the art. Fillers and other additives known in the art, such as carbon black, silica, talc, glass, glass fibers, antioxidants, plasticizers, oils,  
25   waxes, coloring agents, and the like may further be added to the compositions before or after molding or shaping. The block copolymers can also be used in foams, sealants, coatings, weather strippings, sound absorbers and the like with the appropriate additives known to those of  
30   ordinary skill in the art, such as foaming agents, tackifiers, oils, plasticizers, films and the like.

          The block copolymers of this invention can be represented by the following general formula:

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- 15 -

wherein each A is a polymer segment having an average molecular weight from 100 to 1,000,000 daltons chosen independently from homopolymers consisting of HDPE, homo and copolymers of cyclic olefins, such as

5 polycyclopentene and polynorbornene, and isotactic, atactic, and syndiotactic poly-1-olefins such as atactic-PP, isotactic-PP, syndiotactic-PP; random copolymers of 1-olefins and diolefins such as ethylene-propylene rubber, ethylene-propylene-hexadiene rubber, ethylene-

10 butene rubber, linear low density polyethylenes, such that no adjacent segments are the same polymer composition.

Novel block copolymers of this invention include but

15 are not limited to diblock copolymers such as (HDPE)(EP), (i-PP)(EP), (LLDPE)(a-PP), (HDPE)(a-PP), (LLDPE)(HDPE) and the like, and triblock copolymers such as (HDPE)(EP)(HDPE), (HDPE)(EP)(LLDPE), (LLDPE)(a-PP)(LLDPE), (HDPE)(a-PP)(LLDPE), (i-PP)(EP)(i-PP), (s-

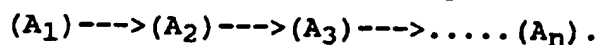
20 PP)(EP)(s-pp) and the like. It will be recognized to those well versed in the field that the isotactic polypropylene segments contained in the block copolymers of this invention have microstructure defects which are not observed in conventional i-PP materials prepared

25 using titanium Ziegler-Natta catalyst. The microstructure defects which are unique to isotactic polypropylenes prepared using metallocene catalysts arise from 1-3 and 2-1 additions to propylene. The melting points of such materials can vary from 60°C to 165°C

30 depending on the total number total defects.

The tapered copolymers can be represented by similar general formula where the transitions between idealized polymer segments  $A_n$  are gradual. These gradient

35 transitions between segments are represented by arrows.



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An example of this would be a polymer prepared by reacting a 50-50 mixture of ethylene and propylene with a living catalyst which has a high preference for ethylene over propylene. The tapered polymer obtained in such an experiment would be designated by the following formula:

HDPE--->EP--->a-PP

The GPC data was obtained on a Waters 150 GPC instrument (MCL, Baytown) equipped with an RI detector. The samples were run at ca. 140°C in trichlorobenzene solvent. The molecular weights were calculated from the PP calibration curves. The thermal behavior of the polymers was recorded by DuPont 912 Differential Scanning Calorimeter. The room temperature and the high temperature tensile properties of polymers were tested on Instron 4505. The polymers were compression molded on a Carver Press into thin sheets and allowed to condition for 24 hours. The micro-tensile specimens were cut and pulled at a crosshead speed of either 2 or 20 in/min. The samples were equilibrated for 5-10 minutes in an environmental chamber prior to testing for high temperature tensile properties. The tension set was measured in terms of % residual strain after holding the sample at 100% strain for 10 minutes followed by relaxation.

Example 1: First Ethylene then Propylene

The reactor was cooled to 0°C and charged with 400 mls of toluene and 0.20 mmoles of catalyst (bis cyclopentadienyl hafnium dimethyl and N,N, dimethylanilinium tetrakis(pentafluorophenyl)boron. Ethylene (4.0 grams; 0.143 moles) was added to 0°C and 2 psig over 25 minutes. After all the ethylene was consumed, propylene (6 grams; 0.139 moles) was added; after 30 minutes the reactor was dropped and the product

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collected. The crude product contained 50 mole % propylene, had a  $M_n = 87,000$  with a molecular weight distribution of 3.0. The crude product was washed with hexane at room temperature to remove any a-PP which was not in the form of block copolymer. The hexane insoluble material contained crystalline HPDE (as determined by IR) and 30 mole % propylene; the  $M_n$  was 144,000 with a molecular weight distribution of 1.89. The hexane soluble fraction was a-PP, did not contain ethylene (by IR), and had a  $M_n$  of 63,000 with a molecular weight distribution of 1.47. Based on the extraction studies, it was concluded that 50-60% of the a-PP chains were incorporated into a block copolymer under these conditions.

#### Example 2: First Propylene then Ethylene

The procedure of Example 1 was repeated except propylene was added first. The crude product had 41 mole % propylene (IR), a  $M_n$  of 170,000 with a molecular weight distribution of 1.78. A pad was pressed and extracted with hexane for 4 hours. At this point, the material contained 37 mole % propylene and very crystalline HDPE. The pad was further extracted with toluene at room temperature for 50 hours with no loss of weight. The extracted "diblock" had a  $M_n$  of 230,000 and a molecular weight distribution of 1.48 (the hexane solubles were a-PP having a  $M_n$  of 125,000 and a molecular weight distribution of 1.72).

#### Example 3: Mw Control in Block Copolymer Synthesis

Using the procedure in Example 2, 3.0 grams of propylene (0.070 moles) were added to 0.20 mmole of the catalyst. After the propylene (0.071 moles) was completely consumed, 2.0 grams of ethylene were added to the system. The resulting product was washed with hexane

at room temperature to remove any a-PP. The resulting block copolymer had a  $M_n$  of 107,000 and a molecular weight distribution of 1.68, and contained 42 mole % propylene by IR spectroscopy.

5

#### Example 4: Effect of Temperature

The procedure of Example 1 was followed except the temperature was varied. If the temperature is raised the effect is to lower the efficiency of the block formation. The temperature was raised from 0°C to 10°C and the blocking efficiency was reduced to less than 10%. When the temperature was lowered to -5°C, the blocking efficiency improved 78%.

15

#### Example 5: Increasing Time Between Monomer Addition

A series of block copolymerizations were run at 0°C and the time between the addition of propylene and ethylene was varied from 6 to 42 minutes. The crude products were collected, analyzed by GPC and IR, then extracted with hexane at room temperature for 65 hours to remove unblocked a-PP. In a well-behaved system wherein the extraction technique removes all of the a-PP, a logarithmically increase in the percent of hexane extractables with time would be expected. The data of this example is shown in Fig. 1 in graphical form. The Y-axis represents the percent of polypropylene which is incorporated into the block copolymer. The extractables were isolated and analyzed by GPC and IR; they were all pure a-PP. The correlation is close to the linear result expected so that this technique can be used to evaluate the kinetics of chain loss under a variety of conditions. This result confirms the ability to make true block c polymers, and confirms that hexane extraction is a good measure of block copolymer efficiency for this polymer system.

Example 6: Preparation of EP

The procedure of Example 1 was followed except where  
5 noted. In this example, 1.6 grams of propylene (0.037  
moles) were added to  $[\text{Cp}_2\text{HfMe}_2][\text{B}(\text{pfp})_4]$  (0.30 mmole) in  
400 cc of toluene at 0°C. Immediately after the  
propylene addition, 1.1 grams of ethylene (0.039 moles)  
was metered in over 3 minutes. After six minutes, the  
10 product was recovered yielding 2.7 grams of amorphous EP  
rubber. The product was non-crystalline by IR; the  
polymer had a  $M_n$  of 96,000 and a molecular weight  
distribution of 1.69.

15 Example 7: Preparation of EP

The procedure of Example 1 was followed except where  
noted. In this example 3.2 grams of propylene (0.074  
moles) was added to  $[\text{Cp}_2\text{HfMe}_2][\text{B}(\text{pfp})_4]$  (0.30 mmole) in  
20 400 cc of toluene at 0°C. Ethylene (2.2 grams; 0.078  
moles) was added to the reactor over 5.5 minutes. The  
product was recovered yielding 5.7 grams of EP rubber  
having a  $M_n$  of 155,000, and molecular weight distribution  
of 1.48. The IR showed some degree of PE-crystallinity.  
25

Example 8: Preparation of EP-b-HDPE

Example 6 was repeated to prepare "living" EP-  
rubber. After all the monomer had been consumed,  
30 ethylene (1.1 grams) was added to prepare the desired  
block copolymer. The product was recovered yielding 4.25  
grams of copolymer. The IR showed PE crystallinity and  
the polymer had thermoplastic-like properties. The onset  
of  $T_g$  was -52.9°C and the product had a melting point of  
35 119°C. The  $M_n$  of the crude product was 161,000 with a  
molecular weight distribution of 1.59.

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Example 9: aPP-HDPE di-Block Copolymer

Blocks were synthesized as follows:

To 400 ml. of toluene containing 0.29 mmoles of  
5  $\text{Cp}_2\text{Hf}(\text{Me})_2$   $\text{DMA}(\text{B}(\text{pfp})_4)$ , 2.3 g. of propylene was added  
first to a two liter zipperclave reactor at 0°C.  
( $\text{DMA}(\text{B}(\text{pfp})_4)$  = N,N-dimethylanilinium terakis  
(pentafluorophenyl) boron.) After 6 minutes of  
polymerization, the pressure dropped to approximately 1  
10 psi. The reactor was then vented through a Nujol  
bubbler. A 5-6 psi vacuum was applied at the end of the  
PP reaction, followed by purging with 20 psi of  $\text{N}_2$ . 20  
psi of  $\text{N}_2$  was charged into the reactor while stirring and  
then vented to aid in removing any remaining propylene  
15 monomer dissolved in the solution. After venting  $\text{N}_2$ , 1.5  
gm. of ethylene was added slowly and allowed 1-3 minutes  
for complete reaction. The resulting polymer was  
precipitated in the methanol and then extracted with  
hexane for 24 hours at room temperature. Soluble aPP was  
20 extracted by hexane whereas HDPE of aPP-HDPE block  
copolymer remained insoluble. Both hexane-soluble and  
insoluble species were then subjected to GPC and FTIR  
analysis for MW and composition. This vacuum/ $\text{N}_2$  purging  
technique produced an end product with a high degree of  
25 HDPE formation. Characterization results are summarized  
in table 1.

Mechanical properties (tensile, elongation, and  
tension set) were also measured for the aPP-HDPE di-block  
30 copolymers made. All measurements were done on an  
Instron model 4505 with crosshead speed set at 20  
inches/minute. Test conditions for the tension set  
measurements were as follows: 100% elongation for 10  
minutes at room temperature, then released. Percent  
35 deformation was measured immediately and after 10  
minutes.

TABLE 1

Table 1 aPP-HDPE Di-Block Copolymers

<u>Charge No. 17005-</u>	<u>87-41</u>	<u>95-45</u>	<u>97-46</u>	<u>101-48</u>	<u>103-49</u>
Yield (gm)	4.87-	4.03	4.04	5.24	4.56
<u>Hexane Insolubles</u>					
wt. %	76	80	86	91	78
PP content, wt. %	36	44	57	49	43
Modulus, psi	1673	2150	2820	2467	2217
Elongation, %	602	400	382	567	476
Tensile, psi	1308	998	933	1345	1134
Tension Set, %	—	46	57	53	59
T <sub>m</sub> , °C	107	108	117	119	116
M <sub>n</sub> , x 1000	218	295	245	255	239
M <sub>w</sub> /M <sub>n</sub>	1.35	1.61	1.54	1.93	1.69
<u>Hexane Solubles</u>					
M <sub>n</sub> , x 1000	—	114	101	112	102
M <sub>w</sub> /M <sub>n</sub>	—	1.76	1.72	2.12	1.6
<u>% C<sub>3</sub> = as aPP</u>	47	36	22	17	40
<u>Cat. Activity</u>					
Mole Di-block/mole cat.	0.059	0.038	0.0049	0.065	0.051
Mole aPP/mole cat.	—	0.025	0.019	0.014	0.034
Active cat. Mole %	—	6.3%	6.8%	7.9%	8.5%



Example 10: HDPE-aPP-HDPE Tri-Blocks

Synthesis of tri-block copolymers was performed under the same conditions as Example 9. In order to avoid precipitation of the first HDPE block in the toluene solution, a small amount of gas phase  $C_3=$  was charged into the reactor and polymerized prior to adding the first block  $C_2=$  monomer. We applied 10 psi vacuum, followed with a 20 psi  $N_2$  purge between each monomer sequence before addition of a new monomer. The final products were precipitated in methanol and dried in a vacuum oven. In order to analyze the product composition, samples were extracted in hexane for 24 hours at room temperature. Block copolymers of HDPE-aPP or HDPE-aPP-HDPE would remain insoluble, whereas aPP would be extracted in this solvent. All soluble as well as insoluble samples were then subjected to MW and compositional analysis by GPC and FTIR. The results for total yields, weight percent of hexane extraction, MW and propylene content are summarized in the following table 2.

Table 2  
HDPE-aPP-HDPE Tri-block Copolymers

	Reac. I (17005-159)	Reac. II (17005-161)	Reac. III (17005-163)
<u>Total Yield (gm)</u>	2.41	6.97	9.03
<u>Hexane insoluble</u>			
wt%	95	59	92
Propylene content, wt%	25.8	51.9	50.4
Modulus, psi	-	2157	2444
Elongation, %	-	670	638
Tensile, psi	-	2398	2256
Tension set, % (10 min at 100%)	-	28	32
Mn, ( $\times 10^{-3}$ )	125	346	331
Mw/Mn	2.1	1.8	2.1
<u>Hexane Soluble</u>			
Mn ( $\times 10^{-3}$ )	-	121	115
Mw/Mn	-	2.4	3.1

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Results of FTIR analysis show that all of the hexane soluble are 100% aPP.

In order to assess the mechanical properties of the linear tri-block copolymers, we synthesized six more samples according to the same reaction conditions as previously described. Table 3 summarizes the data. Samples #51, #53 and #54 were run with block ratios of 1:3:1. Samples #55, #56 and #52 were run with a block ratio of 1:6:1. Sample #52 was run with twice the amount of monomers charged and with the same level of catalyst concentration. We obtained a  $M_n=306,000$  (almost double) with a similar narrow  $M_w/M_n=2.0$ .

Table 3

TABLE 3 HDPE-aPP-HDPE Tri-Block Copolymers

Block Ratio Charge No.	1:3:1			1:6:1		
	51	53	54	55	56	52
Total Yield (gm)	8.87	9.15	8.95	7.43	7.44	13.19
Hexane Insolubles, wt. %	86	79	72	41	47	71
PP content, wt. %	56	64	60	80	74	59
Modulus, psi	1821	1567	2607	859	1243	2933
Elongation, %	676	737	723	810	930	629
Tensile, psi	1630	1638	2039	1198	1625	2171
Tension Set, %	36	24	28	25	19	33
Tm, °C	134	119	121	110/137	119	129
Mn, x 1000	287	293	270	241	207	306
Mw/Mn	1.9	1.9	1.9	1.9	1.9	2.0
Mole. polymer chain/mole. cat.	0.09	0.09	0.08	0.04	0.06	0.11
Hexane Solubles						
Mn, x 1000	171	206	197	222	192	207
Mw/Mn	2.0	2.0	1.9	2.1	2.0	1.9
Mole. polymer chain/mole. cat.	0.03	0.03	0.04	0.07	0.07	0.06
Mole % Active Cat.	0.12	0.12	0.12	0.11	0.13	0.17

Example 11: HDPE-EP-HDPE Tri-block Copolymers

The procedure set out in Example 9 was followed. Three reactions were run with each reaction being terminated at the end of each blocking sequence. Samples of the hexane-soluble and insoluble fractions for each of these reactions were subjected to MW and compositional analysis by GPC and FTIR. Table 4 below summarizes the results.

Table 4			
Reactions	I	II	III
Total Yields(g)	2.06	9.06	9.80
Mn ( $\times 10^{-3}$ )	237	190	299
Mw/Mn	2.05	2.70	2.19
<u>Hexane Insoluble</u>			
Wt%	99.6	36.2	51.8
PP Content, wt%	5.4	*	*
Mn ( $\times 10^{-3}$ )	189	324	297
Mw/Mn	2.28	1.94	2.37
<u>Hexane Solubles**</u>			
Wt%	0.4	63.8	48.2
Mn ( $\times 10^{-3}$ )	-	164	-
Mw/Mn	-	2.44	-

\* The FTIR PP content was too high to be accurately calculated.

\*\* FTIR shows hexane solubles contain both aPP and EP.

Three additional reactions were run using the same reaction conditions as previously described but varying the block ratio and the middle block E/P composition. Table 5 summarizes results from these runs.

Table 5  
HDPE-EP-HDPE Block Copolymers  
 (same reaction conditions as in Example 1)

5	Charge No. 17005-	125-57	127-58	129-59
	Block Ratio, by wt.	1:2.5:1	1:3.6:1	1:13:1
	E/P Ratio, by wt.	1:1	1:6	1:12
	Total Yield, g	7.2	8.2	13.6
10	Exotherm, °C	1	5	20
	<u>Hexane Insolubles</u>			
	Wt %	97	(30)	36
15	Propylene content, wt%	45.9	85.2	-
	Modulus, psi	1560	3107	550
	Elongation, %	509	290	885
	Tensile, psi	1046	1204	688
20	Tension set, % (10; , 100%)	26	45	46
	Mn(K)	510	544	156
	Mw/Mn	1.8	2.1	3.4
	Mol. polymer/ Mol. catalyst	0.047	0.016	0.108
25	<u>Hexane Solubles</u>			
	Wt %	3	70	64
	Mn, 1000	309	470	121
	Mw/Mn	2.0	2.3	4.1
30	Mol. polymer/ Mol. catalyst	0.0024	0.042	0.248

Example 12: EP-RCP Block Copolymers

35 Sequential monomer addition technique was used to  
 synthesize (A) EP-b-RCP Block Copolymers and (B) EP-b-iPP  
 Block Copolymers. (RCP is a tapered or random copolymer  
 of propylene and an alpha olefin preferably ethylene. In  
 the tapered RCP, the polymer chain is amorphous in one  
 40 end and gradually becomes semi-crystalline toward the  
 other end.) Removal of the residual ethylene of the "EP"  
 block by vacuum technique was used to synthesize EP/PP  
 block copolymers consisting of isotactic "PP" block and  
 tapered copolymers (147-1, 149-1, 150-1). The catalyst  
 45 used was MeSi<sub>2</sub>(bis-indeneyl) hafnium dimethyl, indicated  
 in the tables as "Hf-\*", with DMAH(B(pfp)<sub>4</sub>).

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The procedure of example 9 was used except where noted. The polymerization runs were carried out in a 1 L autoclave reactor using toluene diluent. The "EP" block was formed first followed by the "PP" block. In between monomer addition steps the reactor was vented completely (0 psi pressure) or subjected to vacuum/nitrogen purge cycle. The yield was determined by completely drying the crude product in the vacuum oven at 100°C for at least 24 hours. The crude product was then subjected to heptane extraction at RT/50°C for 24 hours. The heptane soluble fraction is the unblocked EP copolymer and heptane insoluble part is EP-b-PP block copolymer.

A. Synthesis and Characterization of EP-block-RCP  
(Random Co-Polymer):

Sequential monomer addition technique was employed. "EP" block was formed first followed by the "PP" block. The reactor was vented in between monomer addition steps. The details of the polymerization conditions and the characterization data of block copolymers are reported in Table 7. A control "EP" run was carried out under similar conditions to simulate "EP" block of EP/PP block copolymer. The crude product obtained in the block run was subjected to the heptane extraction at room temperature.

(B) Synthesis and Characterization of EP-block-iPP:

We followed the procedure in Example 12A above, however, by applying vacuum in between the "EP" and "pp" block, we were able to remove the residual C<sub>2</sub> of "EP" block. The resultant block copolymers exhibited a sharp melting peak in the range of 135-138°C corresponding to the "iPP" block. The polymerization conditions and the characterization of EP-b-iPP block copolymers and tapered copolymers are reported in Table 8 and A. The crude

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product formed in the block run was subjected to heptane extraction at 50°C to insure complete removal of the unblocked EP copolymer. The heptane insoluble fraction was considered to be the block copolymer. The wt% EP in  
5 the block copolymer is calculated from the results obtained in the heptane extraction studies. Mechanical properties are listed in tables 9 and 10.

TABLE

Table A									
ID #	Mole% C <sub>2</sub> In Feed	Polymzn. Temp. (°C)	Polymzn. Time (min.)	Conv. %	Hep. Sol. at RT (Wt%)	Mole% C <sub>2</sub> In Polymer (H NMR)	Mw/MWD (by GPC)	CI (PP) (by FTIR)	
16768-147-1	28	27 to 40	3.0	100	68.0	24	38.4 K/2.9	0.36	
16768-149-1	28	0 to 10	1.5	100	28.0	22	93.8 K/1.8	0.41	
16768-150-1	25	-5 to 5	1.5	100	27.0	20	95.8 K/1.7	0.38	
16768-156-1	33.3	26 to 27	5.0	100	100	30	80.5 K/1.7	0.1	
17450-8-1	33.3	8 to 9	10.0	76	100	34.8	98.8/1.6	0.12	
17450-26-1	33.3	6 to 8	2.0	89	100	32	91.4 K/1.6	0.1	

Conditions: Hf -\*/DMAH-B(pfp)<sub>4</sub> = 0.5 X 10<sup>-4</sup> - 1.0 X 10<sup>-4</sup> moles



TABLE 7

**Synthesis Conditions and Characterization of EP-block-RCP**  
**Conditions: [Hf- $\ast$ ] =  $1.25 \times 10^{-4}$  M [DMAH-B(pfp)<sub>4</sub>] =  $1.25 \times 10^{-4}$  M**

ID #	Run Type	Feed Comp. EP Block (Molar)		C <sub>3</sub> Conc PP Block (Molar)	Polymzn. Time (min.)		Polymzn. Temp. (°C)		Conv. %	Wt% RCP	Mn/MWD	MP (°C)
		[C <sub>2</sub> ]	[C <sub>3</sub> ]		EP	PP	EP	PP				
146-1	EP-PP	0.33	0.825	0.413	1.0	2.0	27 to 41	35	100		35 K/4.2	
146-2		Hep Sol. (7 wt%)									27.3 K/3.9	
146-3		Block(Hep Insol)								30	65 K/2.3	126
147-1	EP	0.33	0.825		3.0		27 to 40		100		38.4 K/2.9	
148-1	EP-PP	0.33	0.825	0.413	1.5	6.0	0 to 7	7	92.4		104.6 K/2.1	
148-2		Hep Sol. (10 wt%)									31.4 K/3.5	
148-3		Block(Hep Insol)								25	125 K/2.0	130
149-1	EP	0.33	0.825		1.5		0 to 10		100		93.8 K/1.8	
151-1	EP-PP	0.33	0.975	0.33	1.5	3.0	-5 to 5	5	100		115.3 K/1.7	
151-2		Hep Sol. (8 wt%)									59.4 K/2.0	
151-3		Block(Hep Insol)								25	128 K/1.6	120
150-1	EP	0.33	0.975		1.5		-5 to 5		100		95.8 K/1.7	

TABLE 8

**Synthesis Conditions (Vacuum Technique Used) and Characterization of EP-block-Iso-PP**  
**Conditions: [HF- $\pi$ ] = 1.0 X 10<sup>-4</sup> moles [DMAH-B(pfp)<sub>4</sub>] = 1.0 X 10<sup>-4</sup> moles**

ID #	Run Type	Feed Comp. EP Block (Molar)		C <sub>3</sub> Conc PP Block (Molar)	Polymzn. Time (min.)		Polymzn. Temp. (°C)		Conv. %	Hep. Sol. @ 50C	Wt% EP (Extra)	Mn/MWD	MP (°C)	
		[C <sub>2</sub> ]	[C <sub>3</sub> ]		EP	PP	EP	PP						
14-1	EP-PP	0.66	0.33	0.66	6	6	1 to 10	9	100	40%	26	126 K/2.3	137	
14-2		Hep. Sol. Block(Hep Insol)										124 K/2.2		
14-3														265 K/2.2
15-1	EP	0.66	0.33	0.66	6		-1 to 7		100	100%	22	91 K/1.7	138	
17-1	EP-PP	0.33	0.165		6	4	12 to 15	14	100	20%				134 K/2.4
17-2		Hep. Sol. Block(Hep Insol)										106 K/2.4		
17-3														344 K/2.1
19-1	EP-PP	0.44	0.22	0.66	6	4	6 to 8	8	93	28%	30	143 K/2.6	137	
19-2		Hep. Sol. Block(Hep Insol)										78 K/1.7		
19-3														224 K/2.0
26-1	EP	0.44	0.22		2		6 to 8		90	100%		92 K/1.6		

TABLE 8 (cont)

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TABLE 9

5	ID #	Stress	% Strain	Tensile	% Strain	Toughness
		@ Yield (psi)	@ Yield	Strength (psi)	@ Break	(in-lb/in <sup>3</sup> )
	14-3	2,364	17	4,221	714	18,220
	17-3	2,883	16	3,264	526	12,160
10	19-3	3,264	13	5,115	714	22,230
	24-3	1,931	19	3,900	774	17,660
	29-3	3,051	16	4,489	700	19,310
15	isoPP Mn = 237 K MWD = 2.16	3,688	12	3,440	470	12,100

20

Table 10

ID #	100% Modulus (psi)	300% Modulus (psi)	Tensile Strength (psi)	% Strain @ Break	% Recovery After 100% Strain
147-1	268	333	1,500	1,320	90
149-1	469	558	1,587	870	85
150-1	427	503	1,750	1,035	85
146-3	859	979	2,734	822	60
148-3	983	1,127	2,616	726	55
151-3	961	1,100	3,100	788	55

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**Claims:**

1. A process for producing block or tapered  
5 copolymers comprising the steps of:

(i) contacting under polymerization conditions in a  
polymerization reactor a first olefinic monomer(s) with  
an activated catalyst complex which is the reaction  
10 product of:

(a) a cyclopentadienyl Group IVB metal component,  
and

15 (b) a second component of an alumoxane or a  
compatible non-coordinating anion to produce a first  
living polymer; and

(ii) sequentially adding to said living polymer at  
20 least a second monomer(s) to copolymerize with said first  
polymer to produce a block or tapered copolymer; and

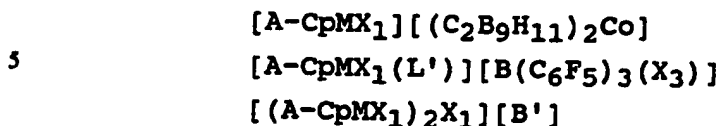
(iii) recovering a block or tapered copolymer having  
a molecular weight distribution of 3 or less.  
25

2. The process of claim 1 wherein the  
polymerization is vented or purged with a dry gas in  
between steps (i) and (ii).

30 3. The process of claim 1 wherein the  
polymerization reactor is vented or subjected to a vacuum  
and purged with a dry gas in between steps (i) and (ii).

4. The process of claim 1, 2 or 3 wherein the  
35 block copolymer is a diblock or triblock copolymer.

5. The process of claim 1 wherein the activated catalyst complex product is represented by the formulae:



wherein: M is titanium, zirconium or hafnium; (A-Cp) is either (Cp)(Cp\*) or Cp-A'-Cp; and Cp and Cp\* are the same or different substituted or unsubstituted cyclopentadienyl radicals; A' is a covalent bridging group containing a Group IV-A element; L' is a neutral Lewis base; X<sub>1</sub> is a hydride radical, hydrocarbyl radical having from 1 to 20 carbon atoms, substituted-hydrocarbyl radical; wherein 1 or more of the hydrogen atoms are replaced with a halogen atom, having from 1 to 20 carbon atoms, or organo-metalloid radical comprising a Group IV-A element wherein each of the hydrocarbyl substituents contained in the organo portion of said organo-metalloid, independently, contain from 1 to 20 carbon atoms; X<sub>3</sub> is a hydride, halide, hydrocarbyl radical, a C<sub>1</sub> - C<sub>20</sub> hydrocarbyl radical wherein one or more of the hydrogen atoms is replaced by a halogen atoms, organometalloid radical wherein each hydrocarbyl substitution in the organic portion contains from 1 to 20 carbon atoms and the metal is a Group IVA metal and B' is a noncoordinating anion.

6. The process of claim 1, wherein the catalyst is the reaction product bis(cyclopentadienyl) hafnium dimethyl and N,N-dimethylanilinium terakis(pentafluorophenyl)boron.

7. The process of claim 1 wherein said steps (i) and (ii) are carried out at a temperature of from -5°C to 10°C.

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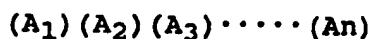
8. The process of claim 1 wherein any f said monomers is selected from the group consisting of ethylene, propylene, and 1-butene.

5 9. The product of the process of claim 1, wherein the product is a tapered copolymer comprising from 15 to 25 mole percent ethylene and having a molecular weight distribution of 2.5 or less.

10 10. The product of the method of claim 1 characterized by a blocking efficiency of 30% or greater.

11. Olefinic block or tapered copolymers having a Mw/Mn 3 or less represented by the formula:

15



wherein n is an integer, each A represent a polymer segment having an average of Mw of from 100 to 1,000,000 daltons and adjacent A's represent different olefinic polymer segments, A being selected from the group consisting of: atactic, syndiotactic or isotactic polymers of one or more of olefins, diolefins,  $\alpha$ -olefins, cyclic olefins and polymers of one or more of olefins, diolefins,  $\alpha$ -olefins, cyclic olefins.

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12. The copolymers of claim 11 wherein each A is selected from atactic-polypropylene, isotactic-polypropylene, syndiotactic-polypropylene, polyethylene, ethylene propylene copolymers, ethylene butene copolymer, ethylene  $\alpha$ -olefin copolymer, HDPE, LLDPE.

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13. The block copolymers of claim 11 wherein said copolymer is a diblock of (HDPE)(EP), (i-PP)(EP), (LLDPE)(a-PP) or (LLDPE)(HDPE) or a triblock of (HDPE)(EP)(HDPE), (HDPE)(EP)(LLDPE), (LLDPE)(a-PP)(LLDPE), (HDPE)(a-pp)(LLDPE) or (i-PP)(EP)(i-PP).

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14. An adhesive comprising block copolymer of claim 11 and a tackifier.

5 15. A molded article or a foam comprising block copolymer of claim 11.



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FIG. 1

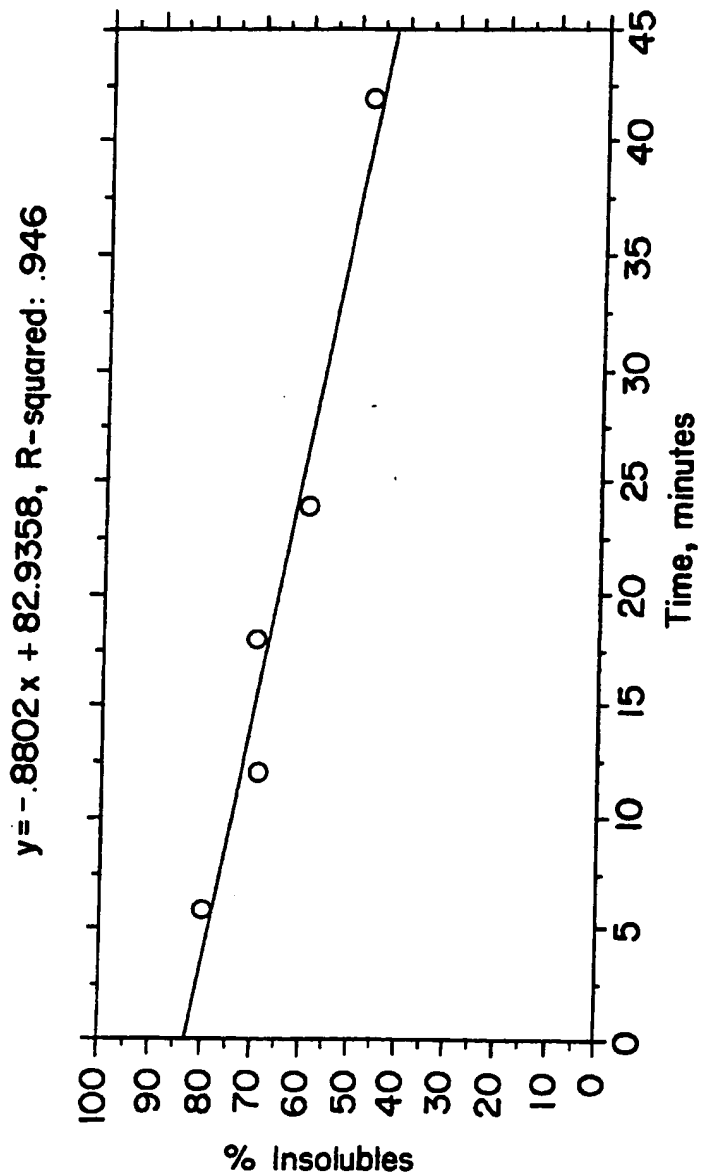
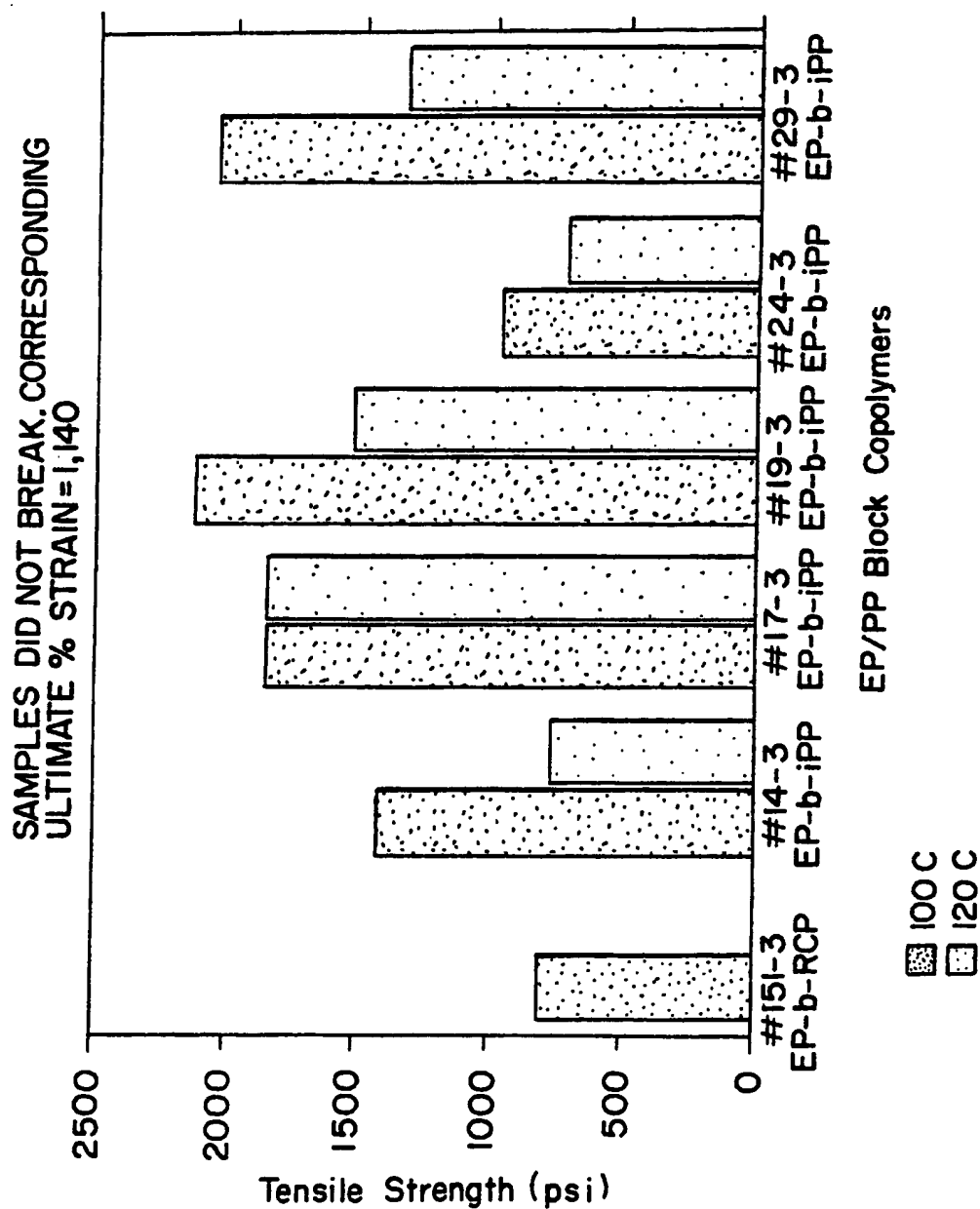
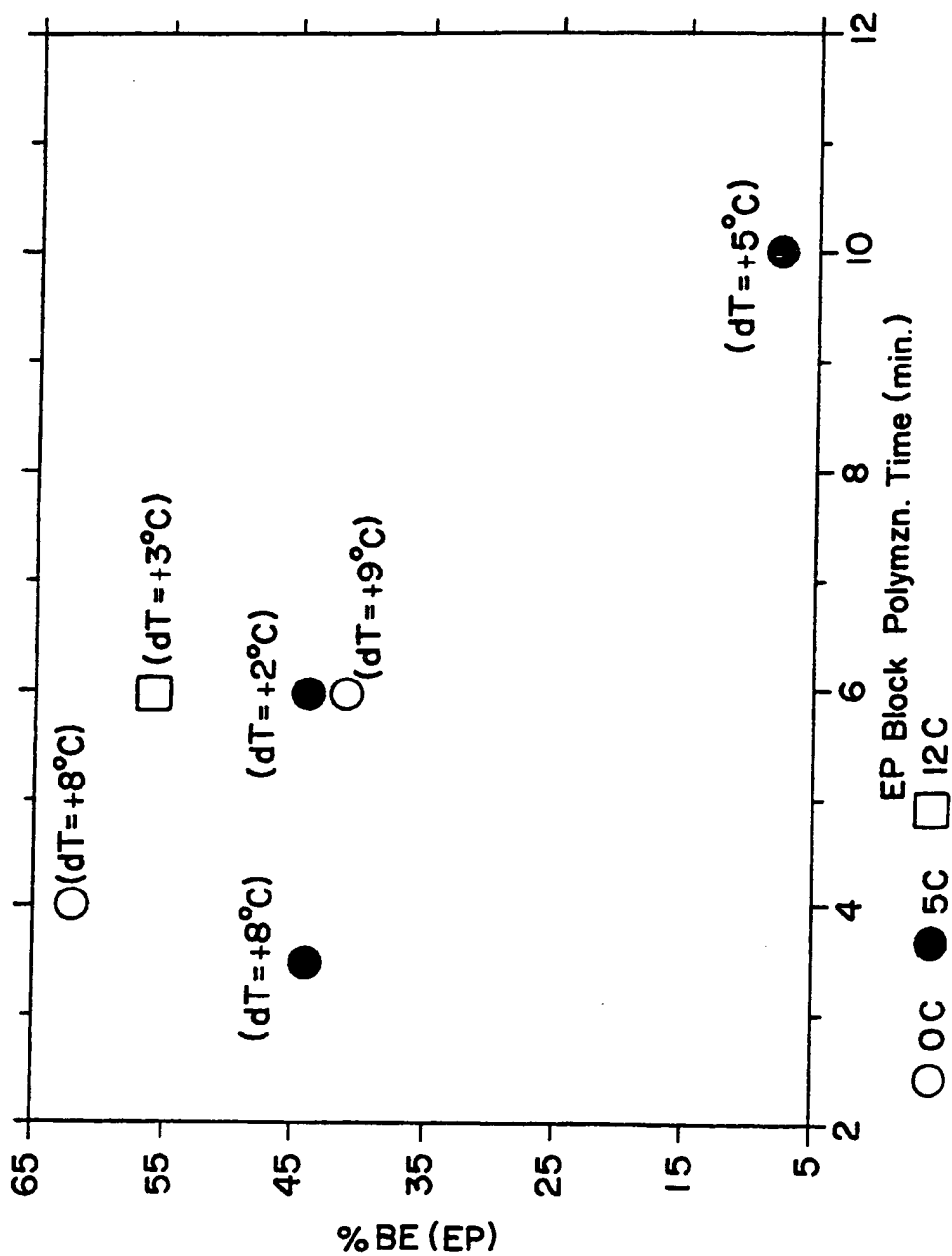


FIG. 2



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FIG. 3



# INTERNATIONAL SEARCH REPORT

International Application No

PCT/US 94/03060

**A. CLASSIFICATION OF SUBJECT MATTER**  
 IPC 5 C08F297/08 C09J153/00

According to International Patent Classification (IPC) or to both national classification and IPC

**B. FIELDS SEARCHED**

Minimum documentation searched (classification system followed by classification symbols)  
 IPC 5 C08F C09J

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practical, search terms used)

**C. DOCUMENTS CONSIDERED TO BE RELEVANT**

Category *	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
X	WO,A,91 12285 (EXXON CHEMICAL PATENTS INC.) 22 August 1991 see page 29, line 22 - page 31, line 22; claims 1-15; examples ---	1-15
X	DE,A,41 30 429 (BASF) 18 March 1993 see claims 1-6; examples; table ---	1
X	EP,A,0 433 986 (HOECHT AG.) 26 June 1991 see claims; example 5 ---	1
A	EP,A,0 433 990 (HOECHST AG.) 26 June 1991 see claims; examples -----	1

☐ Further documents are listed in the continuation of box C.

☒ Patent family members are listed in annex.

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Date of the actual completion of the international search

18 July 1994

Date of mailing of the international search report

- 8. 08. 94

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# INTERNATIONAL SEARCH REPORT

Information on patent family members

International Application No

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